

Zero Dynamics

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Consider system dynamics of the form

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}) + \mathbf{g}(\mathbf{x})\mathbf{u}, \quad (1)$$

where $\mathbf{x} = [\mathbf{q}, \dot{\mathbf{q}}]^T$, and an output of the form

$$\mathbf{y} = \mathbf{h}(\mathbf{q}), \quad (2)$$

which depends only on configuration variables. Because setting $\mathbf{h}(\mathbf{q})$ can only provide constraints on the M actuated degrees of freedom, there exists a smooth real-valued function $\boldsymbol{\theta}(\mathbf{q})$ for the $(N - M)$ unactuated degrees of freedom such that

$$[\mathbf{h}(\mathbf{q}); \boldsymbol{\theta}(\mathbf{q})] : \tilde{\mathcal{Q}} \rightarrow \mathcal{R}^N \quad (3)$$

is a diffeomorphism onto its image. Then the corresponding zero dynamics manifold $T\tilde{\mathcal{Q}}$ is a smooth $2(N - M)$ -dimensional embedded submanifold of $T\mathcal{Q}$, defined as

$$\mathcal{Z} = \{\mathbf{x} \in T\tilde{\mathcal{Q}} | \mathbf{y} = \mathbf{h}(\mathbf{x}) = 0, \dot{\mathbf{y}} = L_{\mathbf{f}}\mathbf{h}(\mathbf{x}) = 0\} \quad (4)$$

Note that because

$$\begin{aligned} \frac{d\mathbf{y}}{dt} &= \frac{d\mathbf{h}}{dt} = \frac{d\mathbf{h}}{d\mathbf{x}} \frac{d\mathbf{x}}{dt} = \frac{d\mathbf{h}}{d\mathbf{x}} \dot{\mathbf{x}} = \begin{bmatrix} \frac{\partial \mathbf{h}}{\partial \mathbf{q}} & \frac{\partial \mathbf{h}}{\partial \dot{\mathbf{q}}} \end{bmatrix} \dot{\mathbf{x}} = \begin{bmatrix} \frac{\partial \mathbf{h}}{\partial \mathbf{q}} & \mathbf{0} \end{bmatrix} \dot{\mathbf{x}} \\ &= L_{\mathbf{f}}\mathbf{h}(\mathbf{q}, \dot{\mathbf{q}}) = \frac{\partial \mathbf{h}}{\partial \mathbf{q}} \dot{\mathbf{q}}, \end{aligned} \quad (5)$$

and

$$\begin{aligned} \frac{d^2\mathbf{y}}{dt^2} &= \frac{d}{dt} \left(\frac{d\mathbf{y}}{dt} \right) = \frac{d}{dt} \left(\frac{\partial \mathbf{h}}{\partial \mathbf{q}} \dot{\mathbf{q}} \right) = \frac{d}{d\mathbf{x}} \left(\frac{\partial \mathbf{h}}{\partial \mathbf{q}} \dot{\mathbf{q}} \right) \dot{\mathbf{x}} = \begin{bmatrix} \frac{\partial}{\partial \mathbf{q}} \left(\frac{\partial \mathbf{h}}{\partial \mathbf{q}} \dot{\mathbf{q}} \right) & \frac{\partial}{\partial \dot{\mathbf{q}}} \left(\frac{\partial \mathbf{h}}{\partial \mathbf{q}} \dot{\mathbf{q}} \right) \end{bmatrix} \dot{\mathbf{x}} = \begin{bmatrix} \frac{\partial}{\partial \mathbf{q}} \left(\frac{\partial \mathbf{h}}{\partial \mathbf{q}} \dot{\mathbf{q}} \right) & \frac{\partial \mathbf{h}}{\partial \mathbf{q}} \end{bmatrix} \dot{\mathbf{x}} \\ &= L_{\mathbf{f}}^2\mathbf{h}(\mathbf{q}, \dot{\mathbf{q}}) + L_{\mathbf{g}}L_{\mathbf{f}}\mathbf{h}(\mathbf{q})\mathbf{u}, \end{aligned} \quad (6)$$

where L stands for the Lie derivative, the relative degree of the output is at least two and thus $\dot{\mathbf{y}} = 0$ is needed in the definition of zero dynamics. The corresponding feedback control \mathbf{u} can be decomposed into two parts as

$$\mathbf{u} = \mathbf{u}^* + \mathbf{v}, \quad (7)$$

where \mathbf{u}^* is the term that renders \mathcal{Z} invariant, *i.e.* $\ddot{\mathbf{y}} = 0$, defined as

$$\mathbf{u}^*(\mathbf{x}) = -(L_{\mathbf{g}}L_{\mathbf{f}}\mathbf{h}(\mathbf{q}))^{-1}L_{\mathbf{f}}^2\mathbf{h}(\mathbf{q}, \dot{\mathbf{q}}) \quad (8)$$

and \mathbf{v} is the term that ensures the output \mathbf{y} and its derivative vanish to zero under the designed control law. A simple example of the control law would be a linear (PD) controller designed in the form

$$\mathbf{v} = -(L_{\mathbf{g}}L_{\mathbf{f}}\mathbf{h}(\mathbf{q}))^{-1} \left[\frac{1}{\epsilon} \mathbf{K}_D L_{\mathbf{f}}\mathbf{h}(\mathbf{q}) + \frac{1}{\epsilon^2} \mathbf{K}_P \mathbf{h}(\mathbf{q}) \right]. \quad (9)$$

To simplify the zero dynamics, further coordinate transformation is performed. Set

$$\Phi(\mathbf{q}) = \begin{bmatrix} \mathbf{h}(\mathbf{q}) \\ \boldsymbol{\theta}(\mathbf{q}) \end{bmatrix} = \begin{bmatrix} \boldsymbol{\eta}_1 \\ \boldsymbol{\xi}_1 \end{bmatrix}, \quad (10)$$

which is a coordinate transformation on $\tilde{\mathcal{Q}}$, thus

$$\begin{bmatrix} \boldsymbol{\eta}_1 \\ \boldsymbol{\xi}_1 \\ \boldsymbol{\eta}_2 \\ \boldsymbol{\xi}_2 \end{bmatrix} = \begin{bmatrix} \boldsymbol{\eta}_1 \\ \boldsymbol{\xi}_1 \\ \dot{\boldsymbol{\eta}}_1 \\ \dot{\boldsymbol{\xi}}_1 \end{bmatrix} = \begin{bmatrix} \mathbf{h}(\mathbf{q}) \\ \boldsymbol{\theta}(\mathbf{q}) \\ L_f \mathbf{h}(\mathbf{q}, \dot{\mathbf{q}}) \\ L_f \boldsymbol{\theta}(\mathbf{q}, \dot{\mathbf{q}}) \end{bmatrix} \quad (11)$$

is a coordinate transformation on $T\tilde{\mathcal{Q}}$, the inverse transformation of which is

$$\begin{bmatrix} \mathbf{q} \\ \dot{\mathbf{q}} \end{bmatrix} = \begin{bmatrix} \Phi^{-1}(\boldsymbol{\eta}_1, \boldsymbol{\xi}_1) \\ \left(\frac{\partial \Phi}{\partial \mathbf{q}}\right)^{-1} \begin{bmatrix} \boldsymbol{\eta}_2 \\ \boldsymbol{\xi}_2 \end{bmatrix} \end{bmatrix}. \quad (12)$$

Note that the above relationship has used the following derivation,

$$\begin{bmatrix} \boldsymbol{\eta}_2 \\ \boldsymbol{\xi}_2 \end{bmatrix} = \begin{bmatrix} \dot{\boldsymbol{\eta}}_1 \\ \dot{\boldsymbol{\xi}}_1 \end{bmatrix} = \frac{d\Phi}{dt} = \frac{\partial \Phi}{\partial \mathbf{q}} \dot{\mathbf{q}} \Rightarrow \dot{\mathbf{q}} = \left(\frac{\partial \Phi}{\partial \mathbf{q}}\right)^{-1} \begin{bmatrix} \boldsymbol{\eta}_2 \\ \boldsymbol{\xi}_2 \end{bmatrix}. \quad (13)$$

Using the new coordinates $[\boldsymbol{\eta}_1; \boldsymbol{\xi}_1; \boldsymbol{\eta}_2; \boldsymbol{\xi}_2]$, the system dynamics become

$$\begin{bmatrix} \dot{\boldsymbol{\eta}}_1 \\ \dot{\boldsymbol{\xi}}_1 \\ \dot{\boldsymbol{\eta}}_2 \\ \dot{\boldsymbol{\xi}}_2 \end{bmatrix} = \begin{bmatrix} L_f \mathbf{h} \\ L_f \boldsymbol{\theta} \\ L_f^2 \mathbf{h} + L_g L_f \mathbf{h} \mathbf{u} \\ L_f^2 \boldsymbol{\theta} + L_g L_f \boldsymbol{\theta} \mathbf{u} \end{bmatrix}, \quad (14)$$

and the zero dynamics become

$$\begin{cases} \mathbf{y} = \boldsymbol{\eta}_1 = \mathbf{0}, \dot{\mathbf{y}} = \dot{\boldsymbol{\eta}}_1 = \boldsymbol{\eta}_2 = \mathbf{0} \\ \dot{\boldsymbol{\xi}}_1 = L_f \boldsymbol{\theta} \\ \ddot{\mathbf{y}} = \dot{\boldsymbol{\eta}}_2 = L_f^2 \mathbf{h} + L_g L_f \mathbf{h} \mathbf{u}^* = \mathbf{0} \\ \dot{\boldsymbol{\xi}}_2 = L_f^2 \boldsymbol{\theta} + L_g L_f \boldsymbol{\theta} \mathbf{u} \end{cases} \Rightarrow \begin{cases} \dot{\boldsymbol{\xi}}_1 = L_f \boldsymbol{\theta} \\ \dot{\boldsymbol{\xi}}_2 = L_f^2 \boldsymbol{\theta} + L_g L_f \boldsymbol{\theta} \mathbf{u} \end{cases}. \quad (15)$$

Because the columns of $\mathbf{g}(\mathbf{x})$ are involutive, the inversion of the decoupling matrix in the zero dynamics can be avoided by using a smooth scalar function $\boldsymbol{\gamma}$, such that

$$\begin{bmatrix} \boldsymbol{\eta}_1 \\ \boldsymbol{\xi}_1 \\ \boldsymbol{\eta}_2 \\ \boldsymbol{\xi}_2 \end{bmatrix} = \begin{bmatrix} \mathbf{h}(\mathbf{q}) \\ \boldsymbol{\theta}(\mathbf{q}) \\ L_f \mathbf{h}(\mathbf{q}, \dot{\mathbf{q}}) \\ \boldsymbol{\gamma}(\mathbf{q}, \dot{\mathbf{q}}) \end{bmatrix} \quad (16)$$

is a valid coordinate transformation and

$$L_g \boldsymbol{\gamma} = \mathbf{0}. \quad (17)$$

Additionally, it can be proved that $\boldsymbol{\gamma}$ can be explicitly computed to be the last $(N - M)$ entry of $\mathbf{D}(\mathbf{q})\dot{\mathbf{q}}$, hence it can be assumed that

$$\boldsymbol{\gamma}(\mathbf{q}, \dot{\mathbf{q}}) = \boldsymbol{\gamma}_0(\mathbf{q})\dot{\mathbf{q}}. \quad (18)$$

The corresponding inverse transformation thus becomes

$$\begin{bmatrix} \mathbf{q} \\ \dot{\mathbf{q}} \end{bmatrix} = \begin{bmatrix} \Phi^{-1}(\boldsymbol{\eta}_1, \boldsymbol{\xi}_1) \\ \left[\frac{\partial \Phi}{\partial \mathbf{q}} \right]^{-1} \begin{bmatrix} \boldsymbol{\eta}_2 \\ \boldsymbol{\xi}_2 \end{bmatrix} \\ \gamma_0 \end{bmatrix}. \quad (19)$$

Consequently, the system dynamics become

$$\begin{bmatrix} \dot{\boldsymbol{\eta}}_1 \\ \dot{\boldsymbol{\xi}}_1 \\ \dot{\boldsymbol{\eta}}_2 \\ \dot{\boldsymbol{\xi}}_2 \end{bmatrix} = \begin{bmatrix} L_f \mathbf{h} \\ \gamma \\ L_f^2 \mathbf{h} + L_g L_f \mathbf{h} \mathbf{u} \\ L_f \gamma \end{bmatrix}, \quad (20)$$

and the zero dynamics become

$$\begin{cases} \dot{\boldsymbol{\xi}}_1 = \gamma \\ \dot{\boldsymbol{\xi}}_2 = L_f \gamma \end{cases}, \quad (21)$$

where the corresponding inverse transformation becomes

$$\begin{bmatrix} \mathbf{q} \\ \dot{\mathbf{q}} \end{bmatrix} = \begin{bmatrix} \Phi^{-1}(\mathbf{0}, \boldsymbol{\xi}_1) \\ \left[\frac{\partial \mathbf{h}}{\partial \mathbf{q}} \right]^{-1} \begin{bmatrix} \mathbf{0} \\ \boldsymbol{\xi}_2 \end{bmatrix} \\ \gamma_0 \end{bmatrix}. \quad (22)$$

To relate the zero dynamics to the original system dynamics, further derivation can be conducted. Set the last $(N - M)$ rows of matrices and vectors \mathbf{D} , \mathbf{C} , \mathbf{G} and \mathbf{q} as \mathbf{D}_M , \mathbf{C}_M , \mathbf{G}_M and \mathbf{q}_M . Then we can have

$$\gamma(\mathbf{q}, \dot{\mathbf{q}}) = \gamma_0(\mathbf{q}) \dot{\mathbf{q}} = \mathbf{D}_M \dot{\mathbf{q}} = \left(\frac{\partial K}{\partial \dot{\mathbf{q}}_M} \right)^T. \quad (23)$$

Therefore, the zero dynamics become

$$\begin{cases} \boldsymbol{\xi}_1 = \boldsymbol{\theta} \\ \boldsymbol{\xi}_2 = \left(\frac{\partial K}{\partial \dot{\mathbf{q}}_M} \right)^T \end{cases} \quad (24)$$

and

$$\left\{ \begin{aligned} \dot{\boldsymbol{\xi}}_1 &= \frac{\partial \boldsymbol{\theta}}{\partial \mathbf{q}} \dot{\mathbf{q}} = \frac{\partial \boldsymbol{\theta}}{\partial \mathbf{q}} \left[\frac{\partial \mathbf{h}}{\partial \mathbf{q}} \right]^{-1} \begin{bmatrix} \mathbf{0} \\ \boldsymbol{\xi}_2 \end{bmatrix} \\ \dot{\boldsymbol{\xi}}_2 &= \left[\frac{\partial(\mathbf{D}_M \dot{\mathbf{q}})}{\partial \mathbf{q}} \quad \frac{\partial(\mathbf{D}_M \dot{\mathbf{q}})}{\partial \dot{\mathbf{q}}} \right] \begin{bmatrix} \dot{\mathbf{q}} \\ -\mathbf{D}^{-1}[\mathbf{C} \dot{\mathbf{q}} + \mathbf{G}] \end{bmatrix} \\ &= \left[\dot{\mathbf{q}}^T \frac{\partial \mathbf{D}_M^T}{\partial \mathbf{q}} \quad \mathbf{D}_M \right] \begin{bmatrix} \dot{\mathbf{q}} \\ -\mathbf{D}^{-1}[\mathbf{C} \dot{\mathbf{q}} + \mathbf{G}] \end{bmatrix} \\ &= \dot{\mathbf{q}}^T \frac{\partial \mathbf{D}_M^T}{\partial \mathbf{q}} \dot{\mathbf{q}} - \mathbf{C}_M \dot{\mathbf{q}} - \mathbf{G}_M \\ &= \dot{\mathbf{q}}^T \frac{\partial \mathbf{D}_M^T}{\partial \mathbf{q}} \dot{\mathbf{q}} - \left(\dot{\mathbf{q}}^T \frac{\partial \mathbf{D}_M^T}{\partial \mathbf{q}} - \frac{1}{2} \dot{\mathbf{q}}^T \frac{\partial \mathbf{D}}{\partial \mathbf{q}_M} \right) \dot{\mathbf{q}} - \mathbf{G}_M \\ &= \frac{1}{2} \dot{\mathbf{q}}^T \frac{\partial \mathbf{D}}{\partial \mathbf{q}_M} \dot{\mathbf{q}} - \mathbf{G}_M \\ &= -\mathbf{G}_M \quad (\text{Because } \mathbf{D} \text{ is related to the kinetic energy which has nothing to do with } \mathbf{q}_M) \\ &= -\frac{\partial V}{\partial \mathbf{q}_M} \end{aligned} \right. \quad (25)$$